

SEHS4653

Control System Analysis

Unit 5

Frequency Response Analysis

(Reference: [1] chapter 7.1 to 7.7)

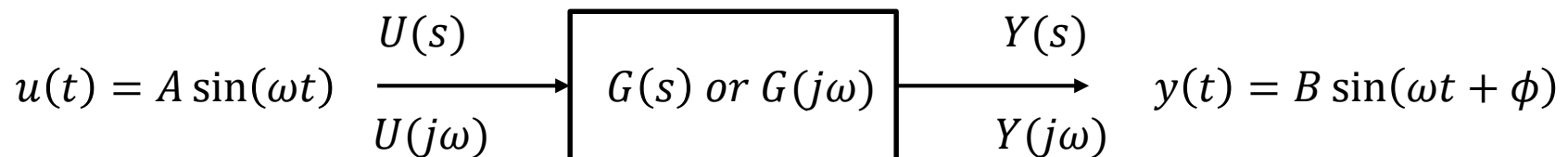
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Introduction

Frequency Response Approach

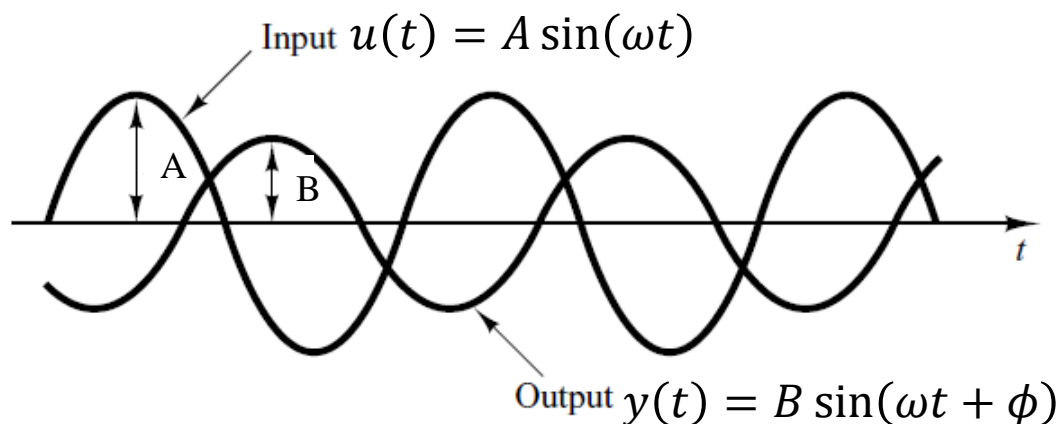
- Steady-state response of a system to a **sinusoidal** input
- Varying the **frequency** of the input signal over a certain range and study the resulting response
- Use the data obtained from measurements (experimentally) on the physical system without deriving its mathematical model (without the transfer function of the control system)
- Replacing s in the transfer function $G(s)$ by $j\omega$, where ω is the frequency
- Graphical forms: **Bode Diagram**, **Nyquist (Polar) Plot** and **Nichols Plot**



ϕ : Phase Shift

Introduction

Frequency Response Approach



$$\frac{Y(j\omega)}{U(j\omega)} = G(j\omega)$$

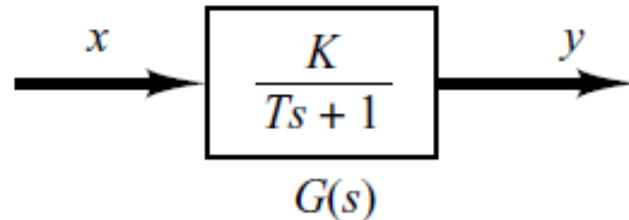
- The function $G(j\omega)$ is called the sinusoidal transfer function, which is a complex quantity
- It can be represented by the magnitude and phase angle with frequency as a parameter

$$|G(j\omega)| = \left| \frac{Y(j\omega)}{U(j\omega)} \right| = \text{amplitude ratio of the output sinusoid to the input sinusoid}$$

$$\angle G(j\omega) = \angle \frac{Y(j\omega)}{U(j\omega)} = \text{phase shift of the output sinusoid with respect to the input sinusoid}$$

Example 1

Consider the system shown below, the transfer function $G(s)$ is



Replacing s in the transfer function $G(s)$ by $j\omega$,

$$G(j\omega) = \frac{K}{j\omega T + 1}$$

The amplitude ratio of the output to the input is,

$$|G(j\omega)| = \frac{K}{\sqrt{(\omega T)^2 + 1^2}} = \frac{K}{\sqrt{1 + \omega^2 T^2}}$$

While the phase angle ϕ is,

$$\angle G(j\omega) = \tan^{-1} \frac{0}{K} - \tan^{-1} \frac{\omega T}{1} = -\tan^{-1} \omega T$$

Bode Diagram

Overview

- Consists of 2 graphs: logarithm of the **magnitude** of a sinusoidal transfer function and **phase angle**
- Both are plotted **against the frequency** on a **logarithmic scale**
- The logarithmic magnitude of $G(j\omega)$ is $20 \log_{10} |G(j\omega)|$ dB (decibels)
- The phase angle (or phase shift) is in degrees or radians
- The curves are drawn on **semilog paper**, using the **log scale for frequency** and the **linear scale** for either **magnitude or phase angle**

Exact Bode Diagram

- Substitute different values of ω (rad/s) into the magnitude and phase angle equations for plotting

Asymptotic Bode Diagram

- Identify basic factors of $G(j\omega)H(j\omega)$ for plotting

Bode Diagram

Basic Factors of $G(j\omega)H(j\omega)$ for plotting Asymptotic Bode Diagram

- Gain K
- Integral $\left(\frac{1}{j\omega}\right)$ and derivative $(j\omega)$ factors
- First-order factors, e.g. $(1 + j\omega T)$ and $\left(\frac{1}{1 + j\omega T}\right)$
- Quadratic factors, e.g. $((j\omega)^2 + 2j\omega\zeta\omega_n + \omega_n^2)$ and $\left(\frac{1}{(j\omega)^2 + 2j\omega\zeta\omega_n + \omega_n^2}\right)$

Bode Diagram (Asymptotic)

The Gain K

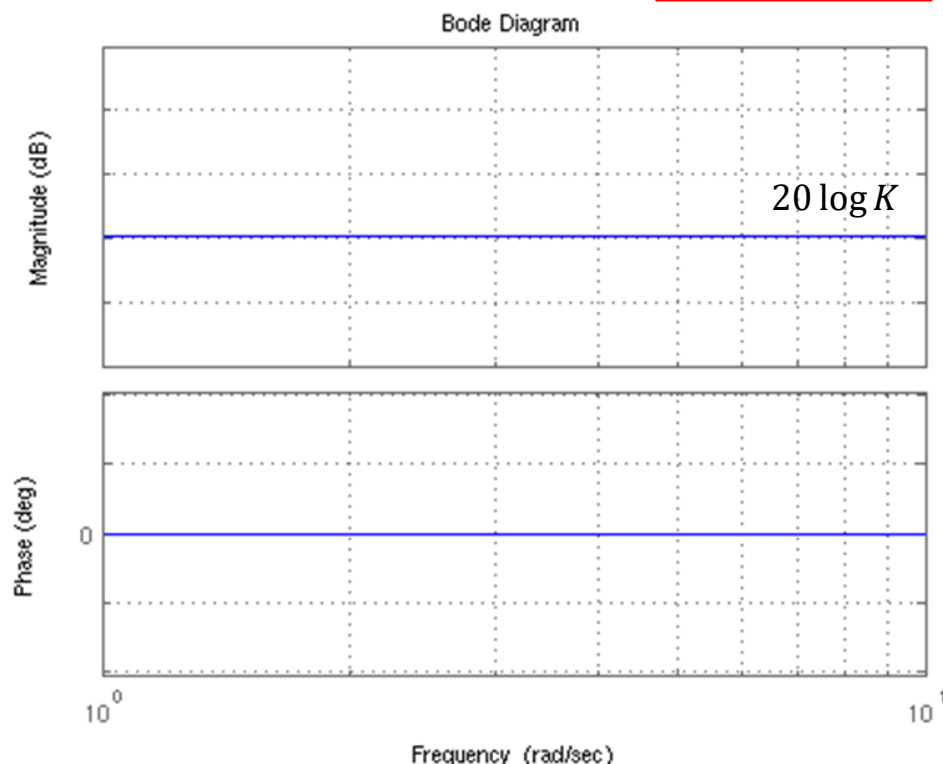
- A number greater than unity has a positive value in decibels, while a number smaller than unity has a negative value
- Consider $G(j\omega) = K$, $K = \text{constant}$

$$G(j\omega) = K$$

Magnitude: $20 \log|G(j\omega)| = 20 \log K$

Phase Angle: $\angle G(j\omega) = \tan^{-1} \frac{0}{K} = 0^\circ$

- The effect of **varying the gain K** in the transfer function is that it **raises or lowers** the **log-magnitude curve** of the transfer function by the corresponding constant amount, but it has **no effect** on the **phase curve**.



Bode Diagram (Asymptotic)

Integral Factor (Pole)

Consider $G(j\omega) = \frac{1}{j\omega}$

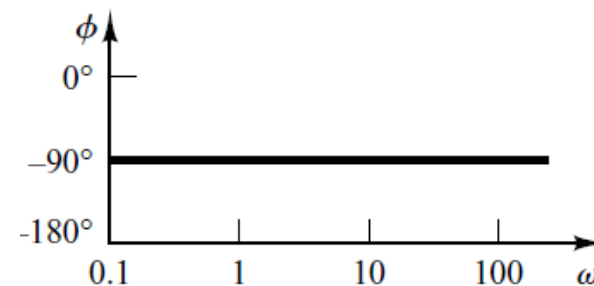
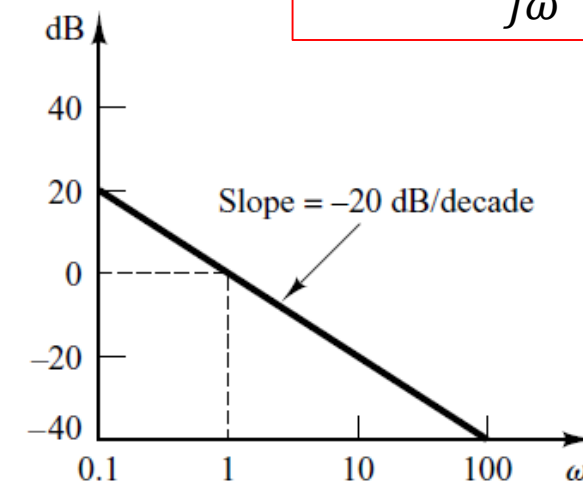
Magnitude: $20 \log \left| \frac{1}{j\omega} \right| = 20 \log \left(\frac{1}{\omega} \right)$

$$= 20 \log \omega^{-1} = -20 \log \omega \text{ (dB)}$$

- The slope of the line is -20 dB / decade

Phase angle: $\angle G(j\omega) = -\tan^{-1} \frac{\omega}{0} = -90^\circ$

$$G(j\omega) = \frac{1}{j\omega}$$



Bode diagram of
 $G(j\omega) = 1/j\omega$

Bode Diagram (Asymptotic)

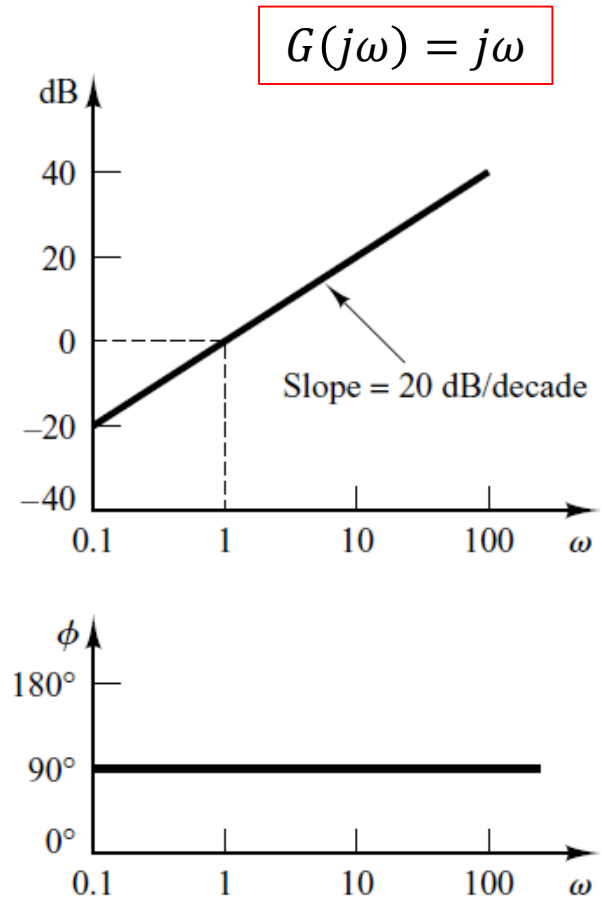
Derivative Factor (Zero)

Consider $G(j\omega) = j\omega$

Magnitude: $20 \log|j\omega| = 20 \log \omega$ (dB)

- The slope of the line is +20 dB / decade

Phase angle: $\angle G(j\omega) = \tan^{-1} \frac{\omega}{0} = +90^\circ$



Bode diagram of
 $G(j\omega) = j\omega$

Bode Diagram (Asymptotic)

First-Order Factors (Pole)

Consider $G(j\omega) = \frac{1}{1+j\omega T}$

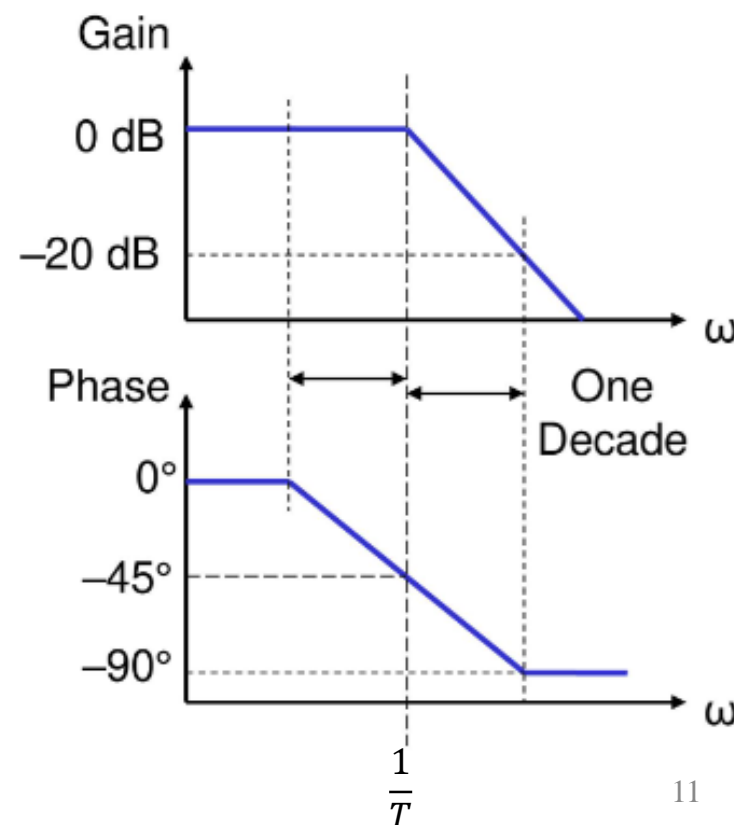
Magnitude: $20 \log|G(j\omega)| = 20 \log \left| \frac{1}{1+j\omega T} \right|$

$$= 20 \log \frac{1}{\sqrt{1^2 + (\omega T)^2}} = -20 \log \sqrt{1 + \omega^2 T^2} \text{ (dB)}$$

Phase angle: $\angle G(j\omega) = \phi = -\tan^{-1} \omega T$

- **At low frequencies**, $\omega \ll 1/T$,
 $-20 \log \sqrt{1 + \omega^2 T^2} \approx -20 \log 1 = 0 \text{ dB}$
- **At high frequencies**, $\omega \gg 1/T$,
 $-20 \log \sqrt{1 + \omega^2 T^2} \approx -20 \log \omega T \text{ dB}$

$$G(j\omega) = \frac{1}{1 + j\omega T}$$



Bode Diagram (Asymptotic)

First-Order Factors (Pole)

The frequency at which the two asymptotes meet is called the **corner frequency** or **break frequency**

- Corner frequency for this example: $\omega = 1/T$
- **At low frequencies**, $\approx -20 \log 1 = 0$ dB
- **At high frequencies**, $\approx -20 \log 10 = -20$ dB
- At $\omega = 0$ rad/s, $\phi = 0^\circ$
- At $\omega \rightarrow \infty$ rad/s, $\phi = -90^\circ$
- At $\omega = 1/T$ rad/s, $\phi = -\tan^{-1} \left(\frac{1}{T} \right) T = -45^\circ$

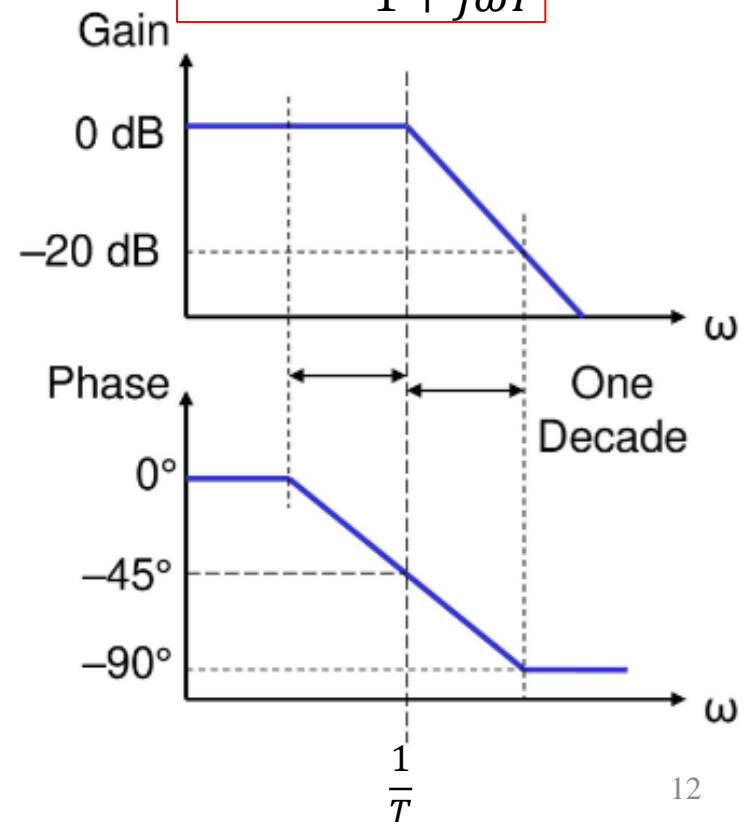
The error in the magnitude curve caused by the use of asymptotes at corner frequency is,

$$-20 \log \sqrt{1 + \left(\frac{1}{T} \right)^2 T^2} = -20 \log \sqrt{2} = -3.01 \text{ dB}$$

$$\text{Magnitude: } -20 \log \sqrt{1 + \omega^2 T^2} \text{ dB}$$

$$\text{Phase: } \angle G(j\omega) = \phi = -\tan^{-1} \omega T$$

$$G(j\omega) = \frac{1}{1 + j\omega T}$$



Bode Diagram (Asymptotic)

First-Order Factors (Zero)

Consider $G(j\omega) = 1 + j\omega T$

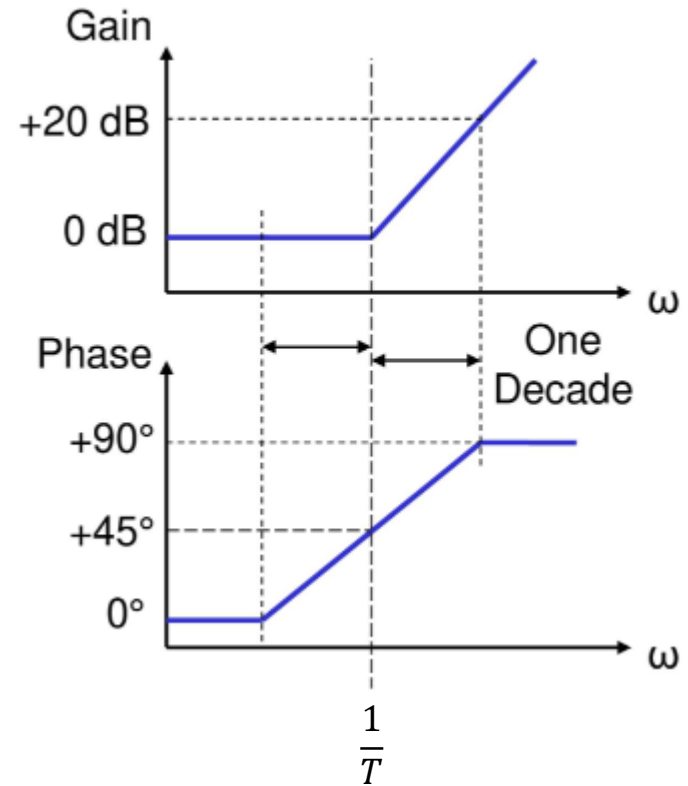
The log-magnitude and the phase-angle curves need only be **changed in sign of the previous case**

Magnitude: $20 \log|G(j\omega)| = 20 \log\sqrt{1^2 + \omega^2 T^2}$ (dB)

Phase angle: $\angle G(j\omega) = \phi = \tan^{-1} \omega T$

The corner frequency is the same

$$G(j\omega) = 1 + j\omega T$$



Bode Diagram (Asymptotic)

Quadratic Factors (Pole)

Consider $G(j\omega) = \frac{1}{(j\omega)^2 + 2j\omega\zeta\omega_n + \omega_n^2}$

$$\therefore G(j\omega) = \frac{1}{1 + 2\zeta \left(j \frac{\omega}{\omega_n}\right) + \left(j \frac{\omega}{\omega_n}\right)^2}$$

- If $\zeta = 1$, this quadratic factor can be expressed as a product of two first-order factors with real poles
- If $0 < \zeta < 1$, this quadratic factor is the product of two complex conjugate factors
- Asymptotic approximations to the frequency-response curves are not accurate for a factor with low values of ζ

$$\text{Magnitude: } 20 \log \left| \frac{1}{1 + 2\zeta \left(j \frac{\omega}{\omega_n}\right) + \left(j \frac{\omega}{\omega_n}\right)^2} \right| = -20 \log \sqrt{\left(1 - \frac{\omega^2}{\omega_n^2}\right)^2 + \left(2\zeta \frac{\omega}{\omega_n}\right)^2}$$

At **low frequencies** such that $\omega \ll \omega_n$, the log-magnitude becomes, $-20 \log 1 = 0$ dB

At **high frequencies** such that $\omega \gg \omega_n$, the log-magnitude becomes,

$$-20 \log \frac{\omega^2}{\omega_n^2} = -40 \log \frac{\omega}{\omega_n} \text{ dB}$$

Bode Diagram

$$G(j\omega) = \frac{1}{1 + 2\zeta \left(j \frac{\omega}{\omega_n}\right) + \left(j \frac{\omega}{\omega_n}\right)^2}$$

Quadratic Factors (Pole)

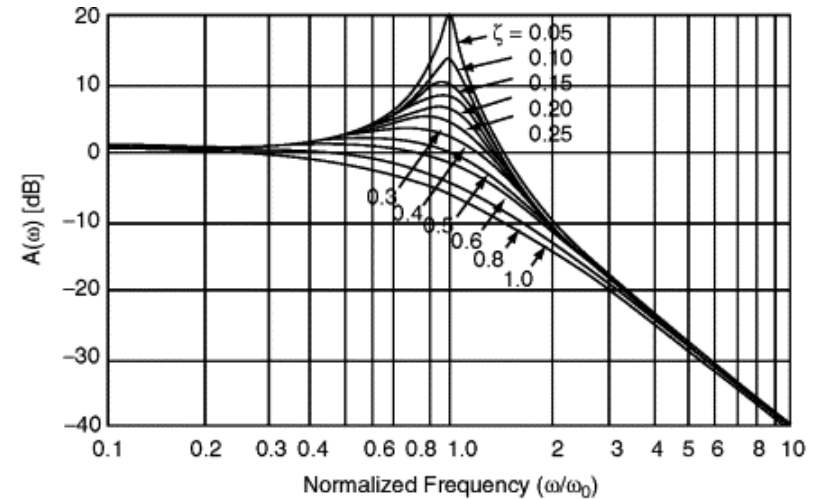
$$\text{Phase: } \phi = -\tan^{-1} \frac{2\zeta \frac{\omega}{\omega_n}}{1 - \left(\frac{\omega}{\omega_n}\right)^2}$$

At $\omega = 0$, the phase angle equals 0°

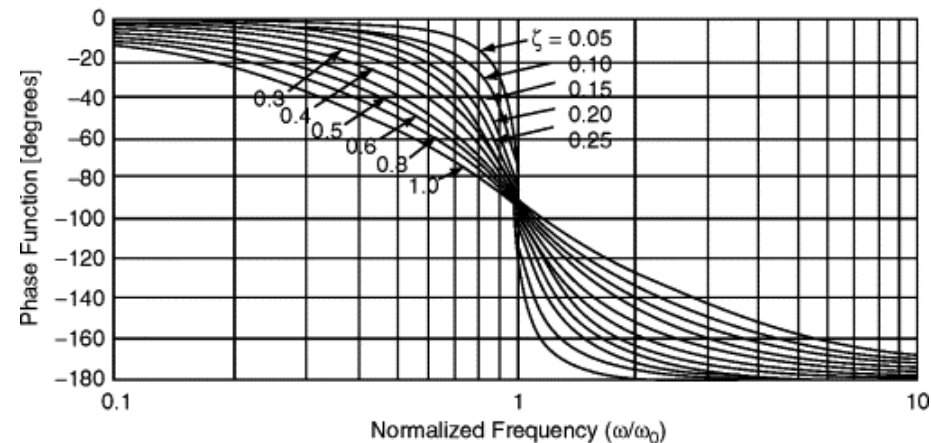
At the corner frequency $\omega = \omega_n$, the phase angle is -90° regardless of ζ ,

$$\phi = -\tan^{-1} \left(\frac{2\zeta}{0} \right) = -\tan^{-1} \infty = -90^\circ$$

At $\omega = \infty$, the phase angle becomes -180°



(A) Magnitude Plot



(B) Phase Plot

Bode Diagram (Asymptotic)

Quadratic Factors (Zero)

Consider $G(j\omega) = (j\omega)^2 + 2j\omega\zeta\omega_n + \omega_n^2 = 1 + 2\zeta \left(j \frac{\omega}{\omega_n} \right) + \left(j \frac{\omega}{\omega_n} \right)^2$

- Similar to the first order factor, merely **reversing the sign** of the log magnitude and that of the phase angle of the factor

$$\text{Magnitude:} \quad = 20 \log \sqrt{\left(1 - \frac{\omega^2}{\omega_n^2}\right)^2 + \left(2\zeta \frac{\omega}{\omega_n}\right)^2}$$

$$\text{Phase:} \quad \phi = \tan^{-1} \frac{2\zeta \frac{\omega}{\omega_n}}{1 - \left(\frac{\omega}{\omega_n}\right)^2}$$

Bode Diagram (Asymptotic)

General Procedure for Plotting Bode Diagrams

- Rewrite the transfer function, $G(j\omega)H(j\omega)$, as a product of the **basic factors** as discussed before
- Identify the **corner frequencies** associated with these basic factors
- Draw the **asymptotic log-magnitude** curves with **proper slopes** between the corner frequencies
- The phase-angle curve can be drawn by **adding** the phase-angle curves of individual factors

Advantages

- Much **less time** than other methods that may be used for computing the frequency response of a transfer function
- The **ease of plotting** the frequency-response curves for a given transfer function and the **ease of modification** as compensation is added are the main reasons

Example 2

Plot the Bode diagram for the transfer function,

$$G(s) = \frac{10}{s + 20}$$

Answer:

Step 1: Replacing s by $j\omega$ and rewrite the transfer function as a product of basic factors

$$G(j\omega) = \frac{10}{j\omega + 20} = \frac{\frac{10}{20}}{\frac{j\omega + 20}{20}} = \frac{1/2}{\frac{j\omega}{20} + 1}$$

Magnitude of the Gain constant = $20 \log\left(\frac{1}{2}\right) = -6.01 \text{ dB}$

Step 2: Identify the corner frequencies

Since there is only one first order factor (Pole), the corner frequency is, $\omega = 20 \text{ rad/s}$

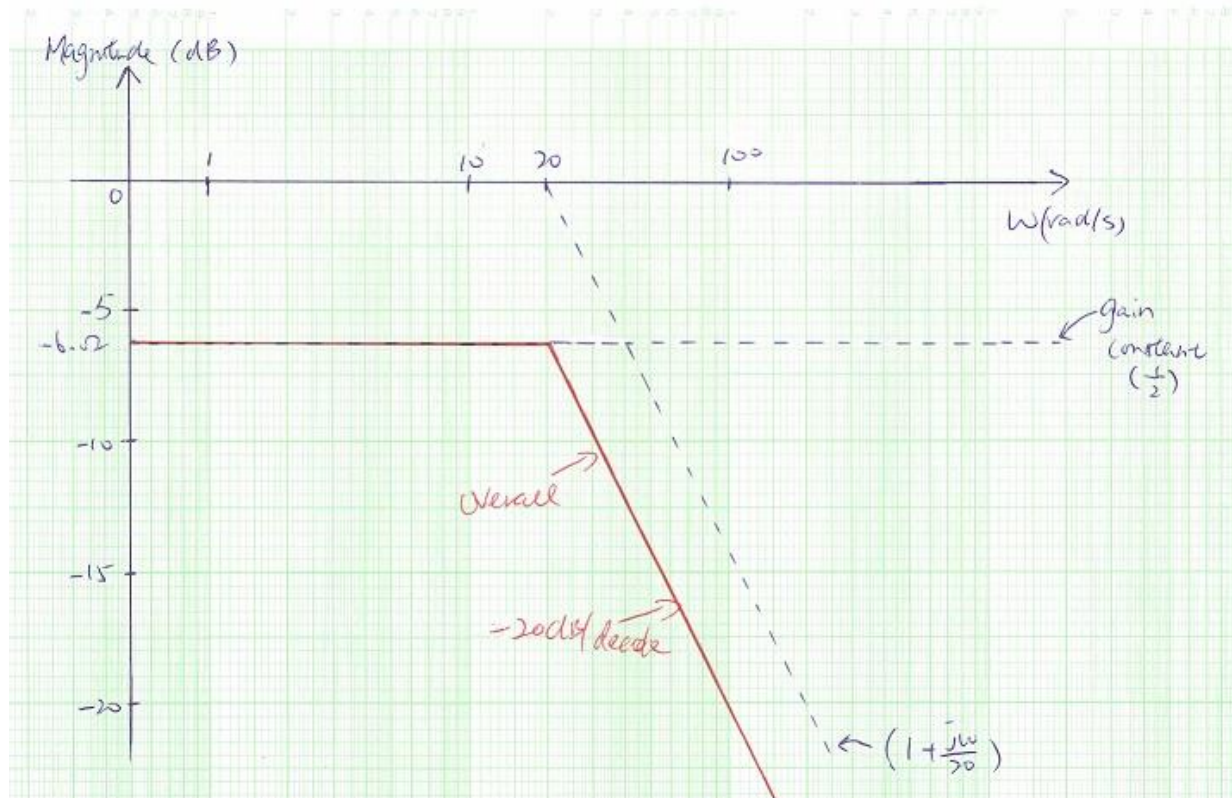
Example 2

$$G(j\omega) = \frac{1/2}{\frac{j\omega}{20} + 1}$$

Answer:

Step 3: Draw the asymptotic log-magnitude and phase-angle curves for individual basic factors

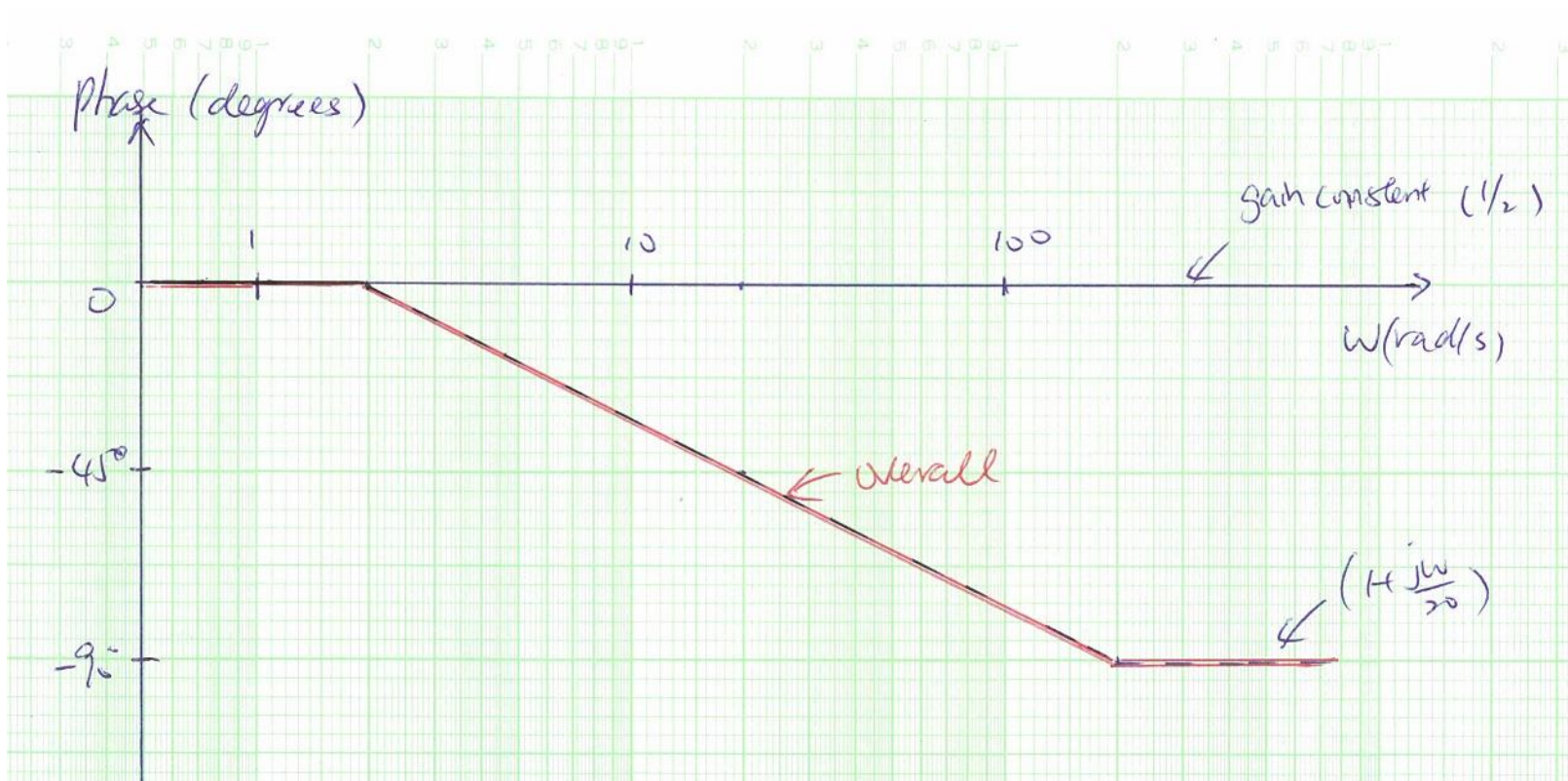
Step 4: Combine the log-magnitude and phase-angle curves



Example 2

$$G(j\omega) = \frac{1/2}{\frac{j\omega}{20} + 1}$$

Answer:



Example 2

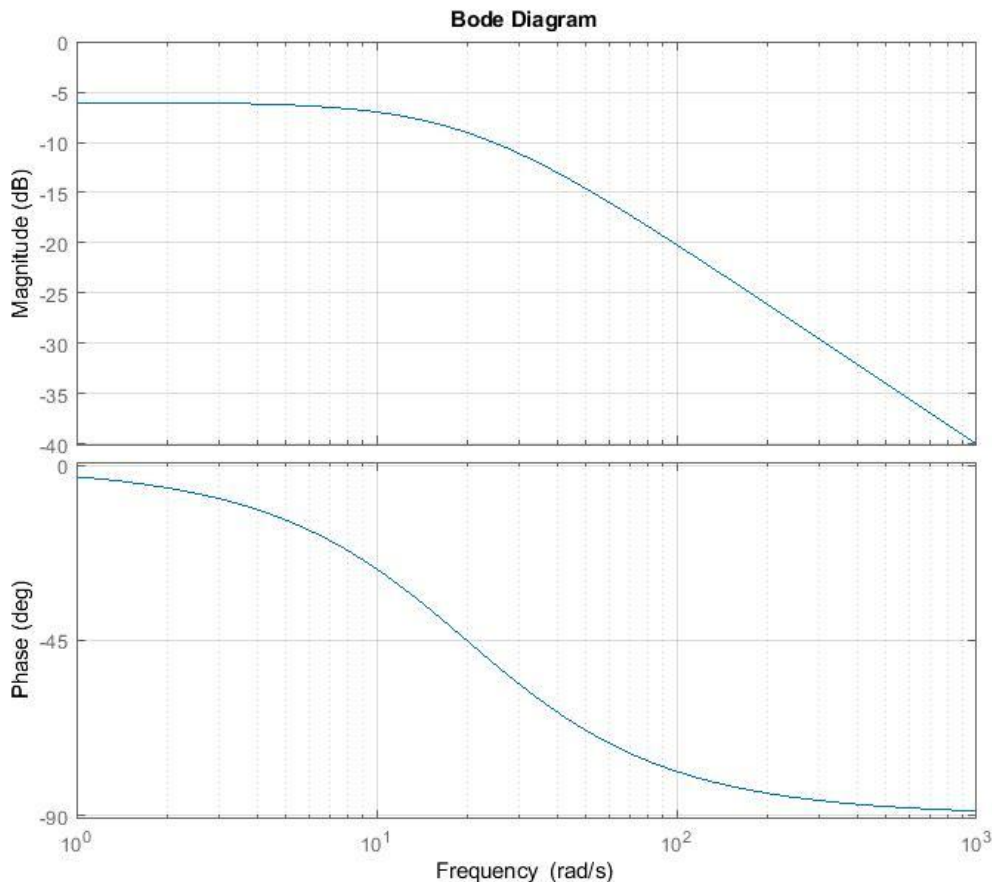
$$G(j\omega) = \frac{10}{j\omega + 20}$$

$$|G(j\omega)| = 20 \log \frac{10}{\sqrt{\omega^2 + 20^2}}$$

$$\angle G(j\omega) = -\tan^{-1} \frac{\omega}{20}$$

Answer:

Exact Bode Diagram from Matlab



ω (rad/s)	$ G(j\omega) $ (dB)	$\angle G(j\omega)$ (°)
1	-6.03	-2.86
3	-6.12	-8.53
5	-6.28	-14.04
10	-6.99	-26.57
20	-9.03	-45
50	-14.62	-68.2
70	-17.24	-74.05
100	-20.17	-78.69
200	-26.06	-84.29
600	-35.57	-88.09
800	-38.06	-88.57
1000	-40	-88.85

Example 3

Plot the Bode diagram for the transfer function,

$$G(s) = \frac{100(s + 1)}{(s + 5)(s + 10)}$$

Answer:

Step 1: Replacing s by $j\omega$ and rewrite the transfer function as a product of basic factors

$$G(j\omega) = \frac{100(j\omega + 1)}{(j\omega + 5)(j\omega + 10)} = \frac{100 \left(\frac{j\omega + 1}{1} \right)}{\left(\frac{j\omega + 5}{5} \right) \left(\frac{j\omega + 10}{10} \right)} \left(\frac{1}{(5)(10)} \right) = \frac{(2)(1 + j\omega)}{\left(1 + \frac{j\omega}{5} \right) \left(1 + \frac{j\omega}{10} \right)}$$

Step 2: Identify the corner frequencies

Corner frequency is, $\omega = 5$ rad/s for the pole $\left(1 + \frac{j\omega}{5} \right)$

Corner frequency is, $\omega = 10$ rad/s for the pole $\left(1 + \frac{j\omega}{10} \right)$

Corner frequency is, $\omega = 1$ rad/s for the zero $(1 + j\omega)$

Magnitude of the Gain
constant

$$= 20 \log(2) = 6.01 \text{ dB}$$

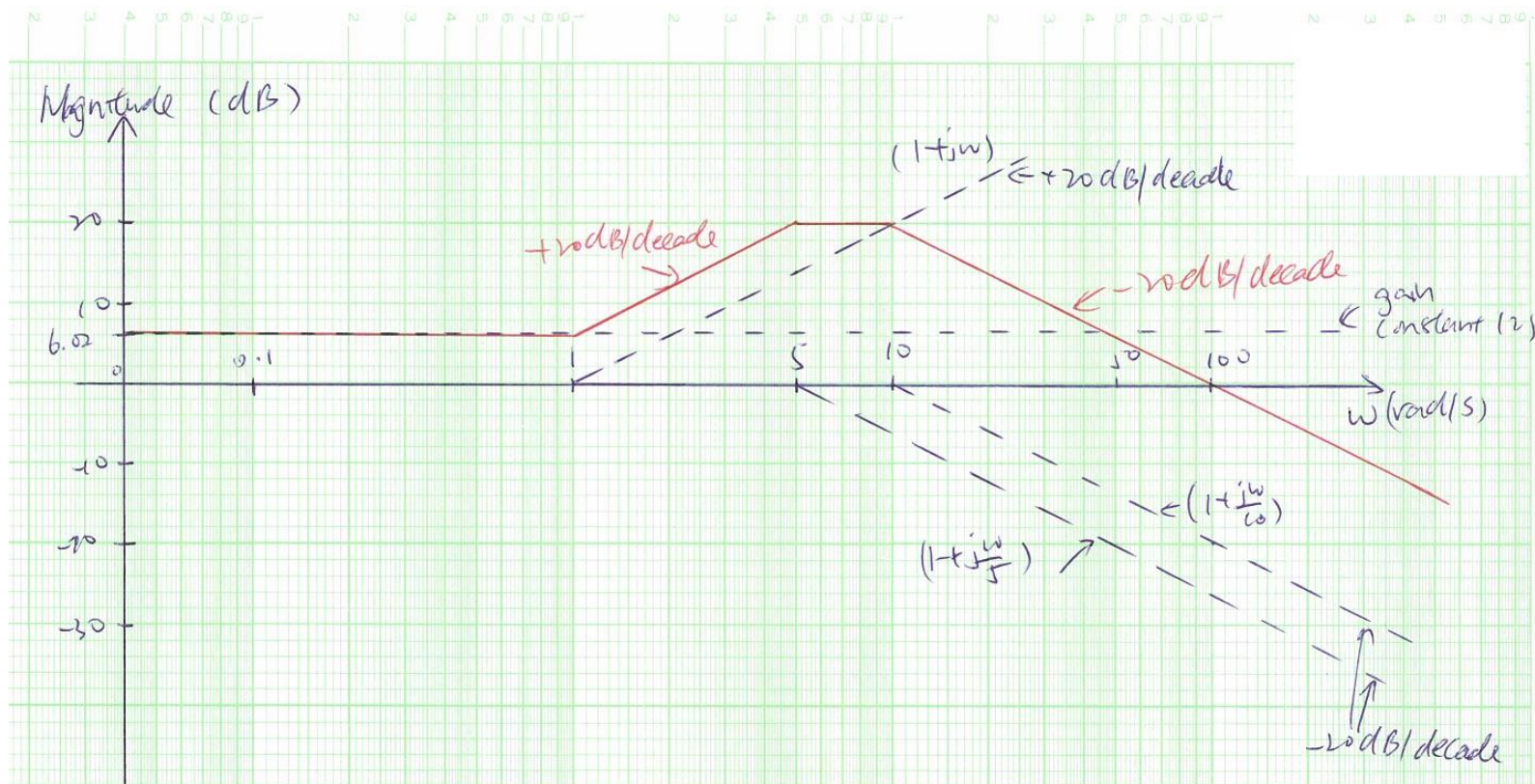
Example 3

$$G(j\omega) = \frac{(2)(1 + j\omega)}{\left(1 + \frac{j\omega}{5}\right)\left(1 + \frac{j\omega}{10}\right)}$$

Answer:

Step 3: Draw the asymptotic log-magnitude and phase-angle curves for individual basic factors

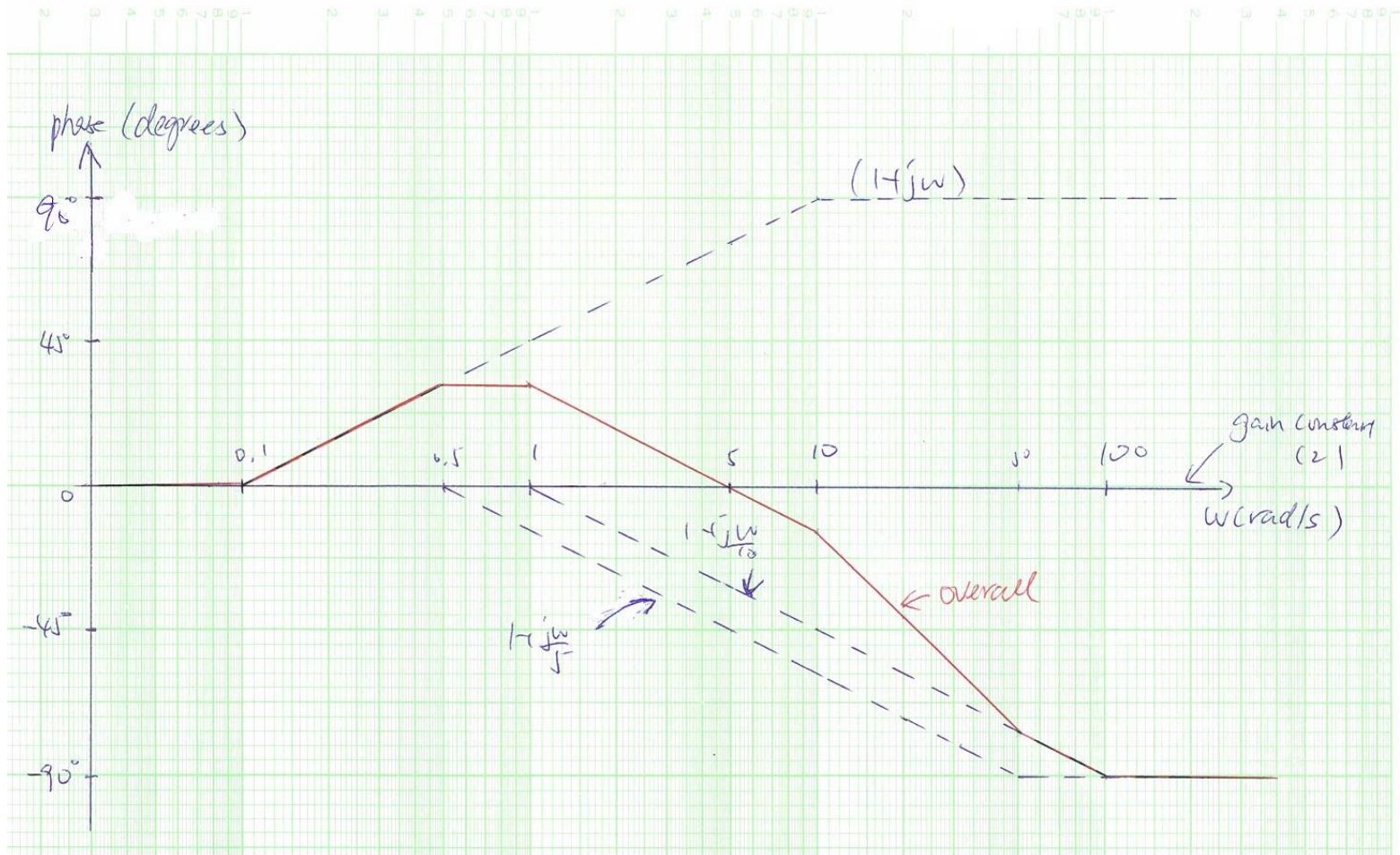
Step 4: Combine the log-magnitude and phase-angle curves



Example 3

$$G(j\omega) = \frac{(2)(1 + j\omega)}{\left(1 + \frac{j\omega}{5}\right)\left(1 + \frac{j\omega}{10}\right)}$$

Answer:



Example 3

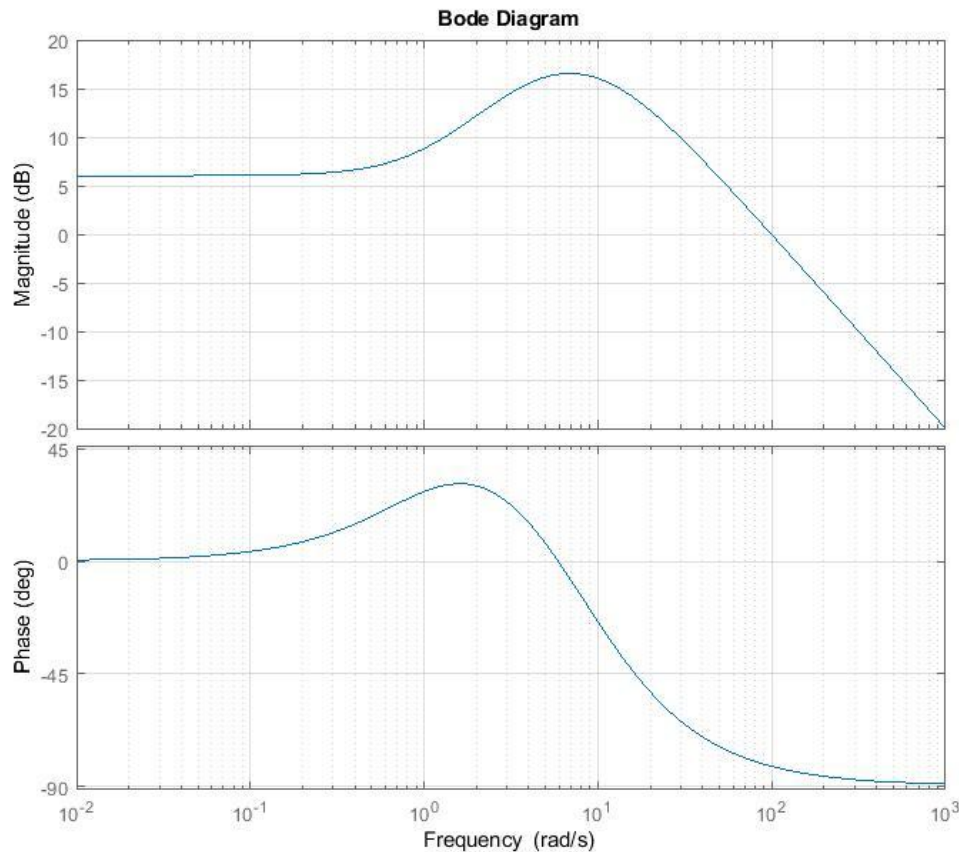
$$G(j\omega) = \frac{100(j\omega + 1)}{(j\omega + 5)(j\omega + 10)}$$

$$|G(j\omega)| = 20 \log \frac{100\sqrt{\omega^2 + 1^2}}{\sqrt{\omega^2 + 5^2}\sqrt{\omega^2 + 10^2}}$$

$$\angle G(j\omega) = \tan^{-1} \omega - \tan^{-1} \frac{\omega}{5} - \tan^{-1} \frac{\omega}{10}$$

Answer:

Exact Bode Diagram from Matlab

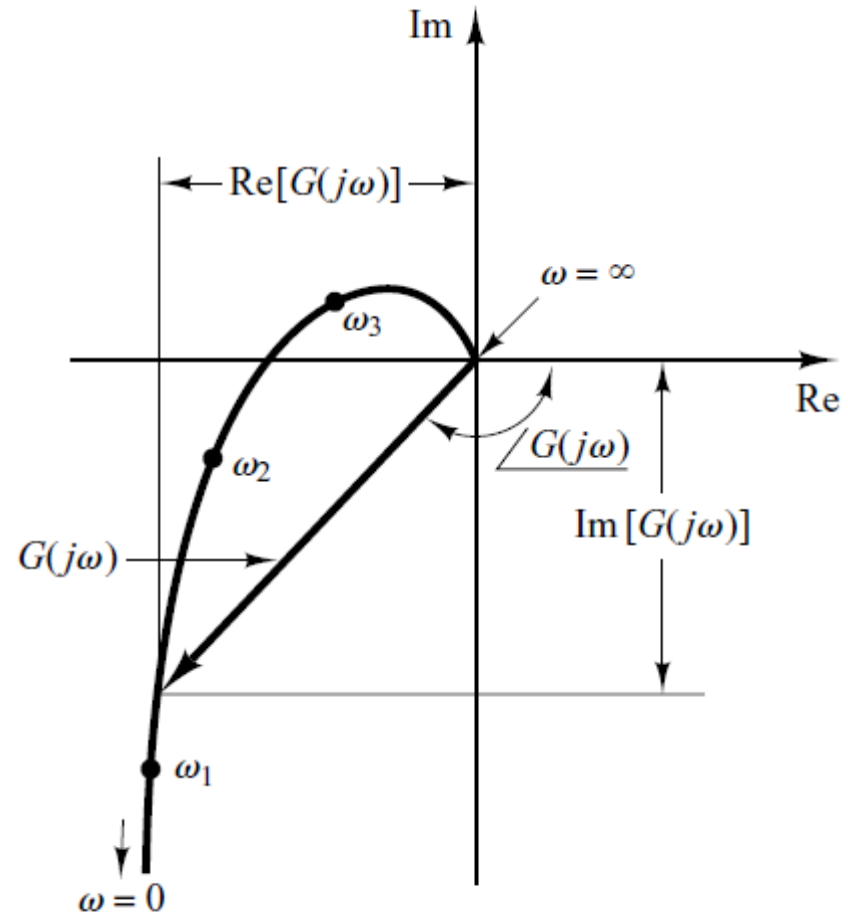


ω (rad/s)	$ G(j\omega) $ (dB)	$\angle G(j\omega)$ (°)
0.1	6.06	3.99
0.5	6.94	17.99
0.8	8.03	25
1	8.82	27.98
3	14.31	23.9
5	16.19	7.13
10	16.06	-24.15
30	9.89	-64.01
50	5.81	-74.13
100	-0.05	-82
500	-13.98	-88.4
1000	-20	-89.2

Polar (or Nyquist) Plot

Overview

- A plot of the **magnitude** of $G(j\omega)$ versus the **phase angle** of $G(j\omega)$ on polar coordinates as ω is varied from **zero to infinity**
- Note that in polar plots a **positive** (**negative**) **phase angle** is measured **counterclockwise** (**clockwise**) from the positive real axis
- Each point on the polar plot of $G(j\omega)$ represents the terminal point of a vector at a particular value of ω
- It depicts the frequency-response characteristics of a system over the **entire frequency range** in a single plot



Example 4

The polar plot of the transfer function,

$$G(s) = \frac{10}{s(s+1)}$$

Answer:

Replacing s into $j\omega$, $G(j\omega) = \frac{10}{j\omega(j\omega+1)}$

Write the expressions for magnitude and phase of $G(j\omega)$ and varies ω from 0 to ∞ .

ω rad/s	M	ϕ
0	∞	-90°
0.5	17.89	-116.57°
1.0	7.071	-135°
2.0	2.236	-153.43°
5.0	0.392	-168.69°
8.0	0.155	-172.87°
10.0	0.995	-174.29°

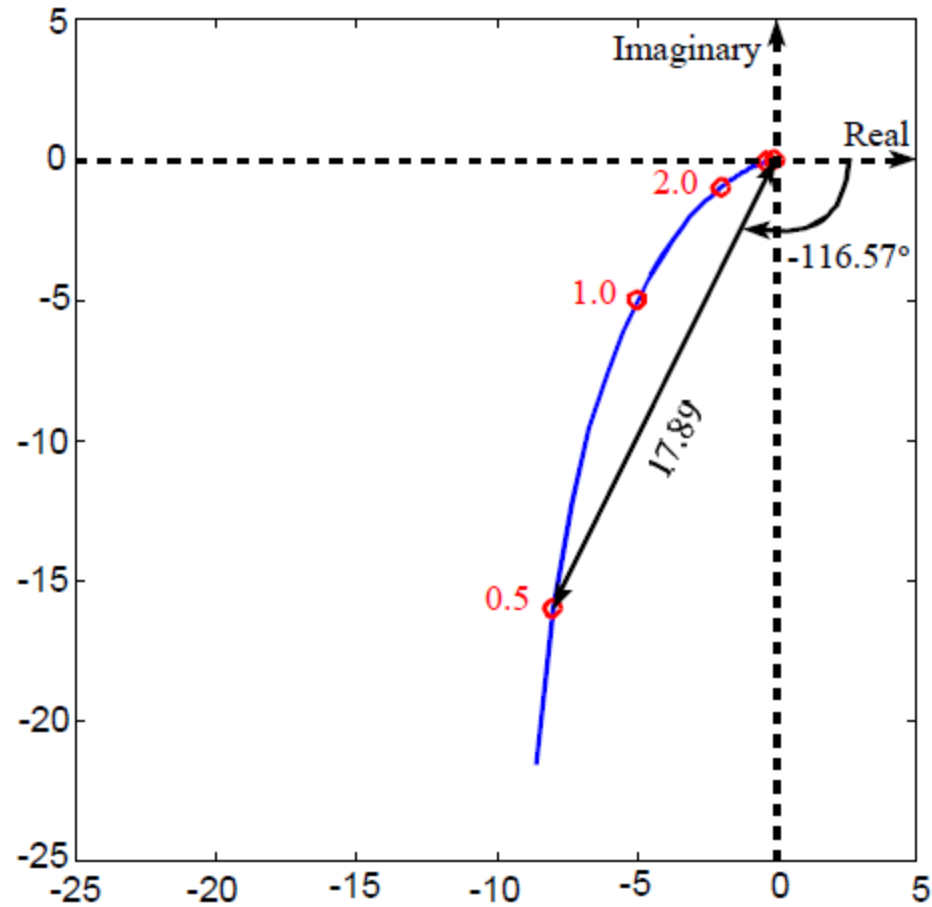
$$M = \frac{10}{\omega\sqrt{\omega^2 + 1^2}}$$

$$\phi = -90^\circ - \tan^{-1} \omega$$

Example 4

Answer:

The polar plot is,



Log-Magnitude-versus-Phase Plot (Nichols Plot)

Overview

- A plot of the **logarithmic magnitude** in decibels **versus the phase angle** or **phase margin** for a frequency range of interest
- The **phase margin** is the difference between the actual phase angle ϕ and -180° ; that is, $\phi - (-180^\circ) = 180^\circ + \phi$
- It combines the 2 curves, log-magnitude curve and the phase-angle curve, in Bode diagrams
- A **change in the gain constant** of $G(j\omega)$ merely shifts the **curve up** (for increasing gain) **or down** (for decreasing gain), but the **shape** of the curve remains the **same**
- The relative stability of the closed-loop system can be determined quickly and that compensation can be worked out easily

Example 5

The Nichols plot of the transfer function,

$$G(s) = \frac{10}{s(s+1)}$$

Answer:

Replacing s into $j\omega$,
$$G(j\omega) = \frac{10}{j\omega(j\omega+1)}$$

Write the expressions for magnitude and phase of $G(j\omega)$ and varies ω from 0 to ∞ .

ω rad/s	M (dB)	ϕ
0	∞	-90°
0.5	25.05	-116.57°
1.0	16.99	-135°
2.0	6.99	-153.43°
5.0	-8.13	-168.69°
8.0	-16.19	-172.87°
10.0	-20.04	-174.29°

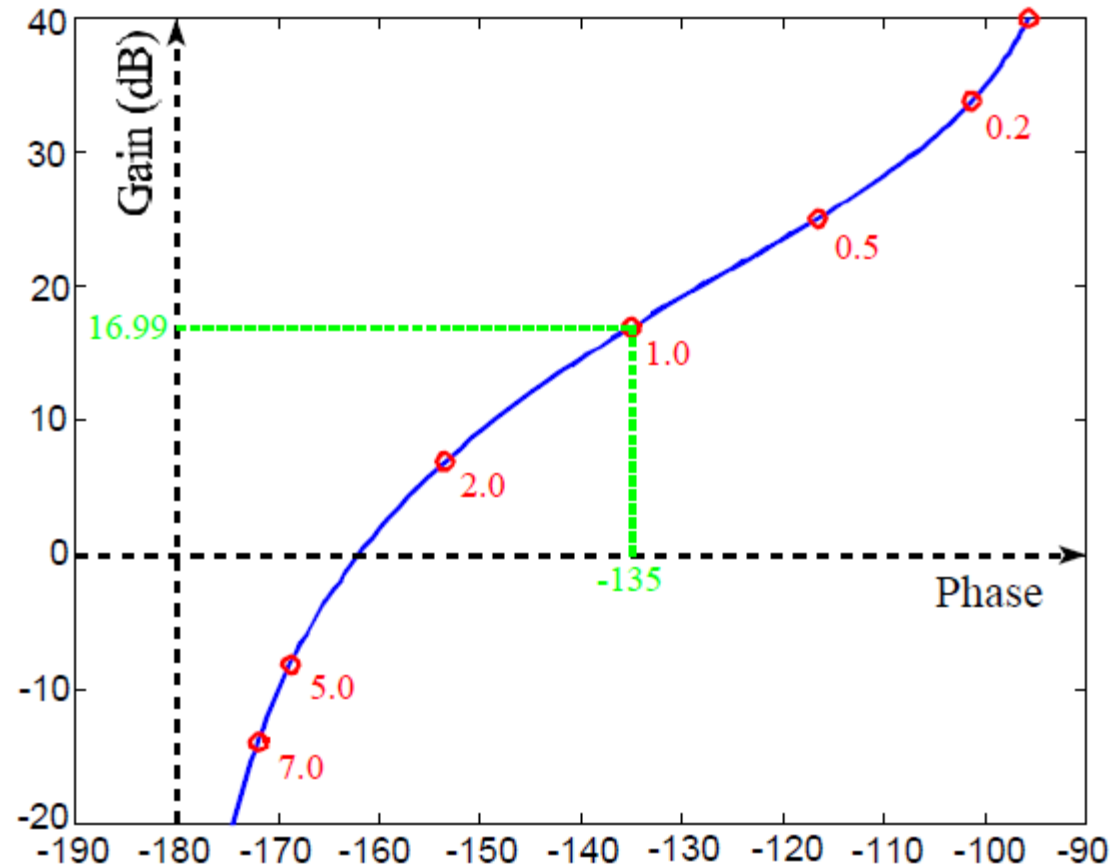
$$\begin{aligned} M &= \frac{10}{\omega\sqrt{\omega^2+1^2}} \\ &= 20 \log 10 - 20 \log \omega \\ &\quad - 20 \log \sqrt{\omega^2+1} \end{aligned}$$

$$\phi = -90^\circ - \tan^{-1} \omega$$

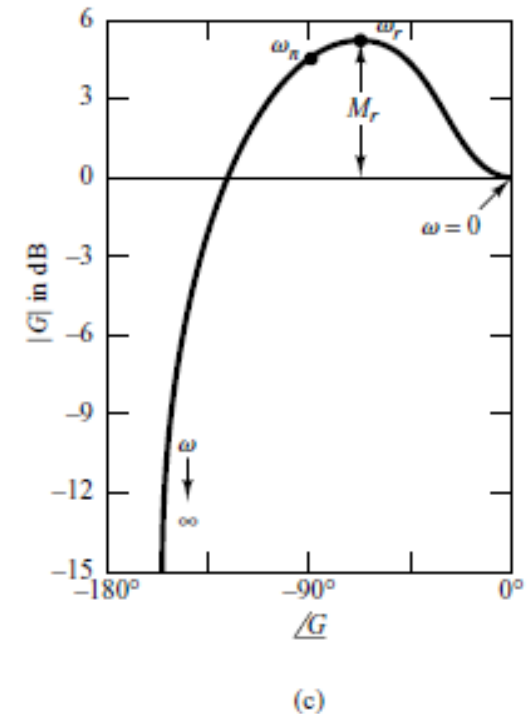
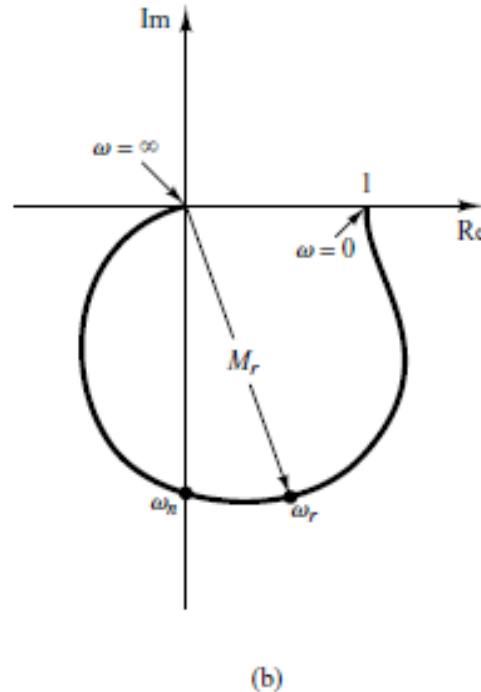
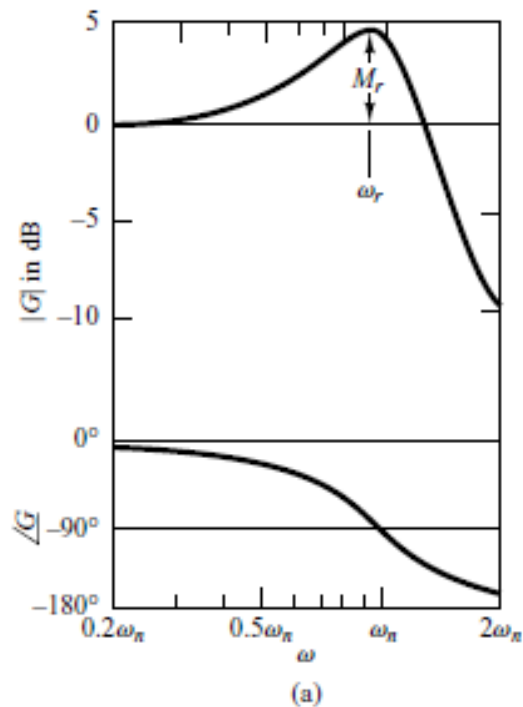
Example 5

Answer:

The Nichols plot is,



Log-Magnitude-versus-Phase Plot (Nichols Plot)



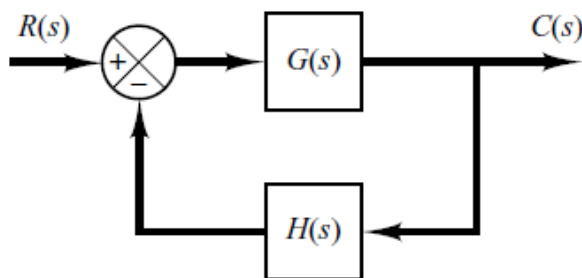
Three representations of the frequency response of $\frac{1}{1 + 2\zeta\left(j\frac{\omega}{\omega_n}\right) + \left(j\frac{\omega}{\omega_n}\right)^2}$, for $\zeta > 0$.

(a) Bode diagram; (b) polar plot; (c) log-magnitude-versus-phase plot.

Nyquist Stability Criterion

Overview

- The Nyquist stability criterion determines the **stability of a closed-loop system** from its **open-loop frequency response** and **open-loop poles**



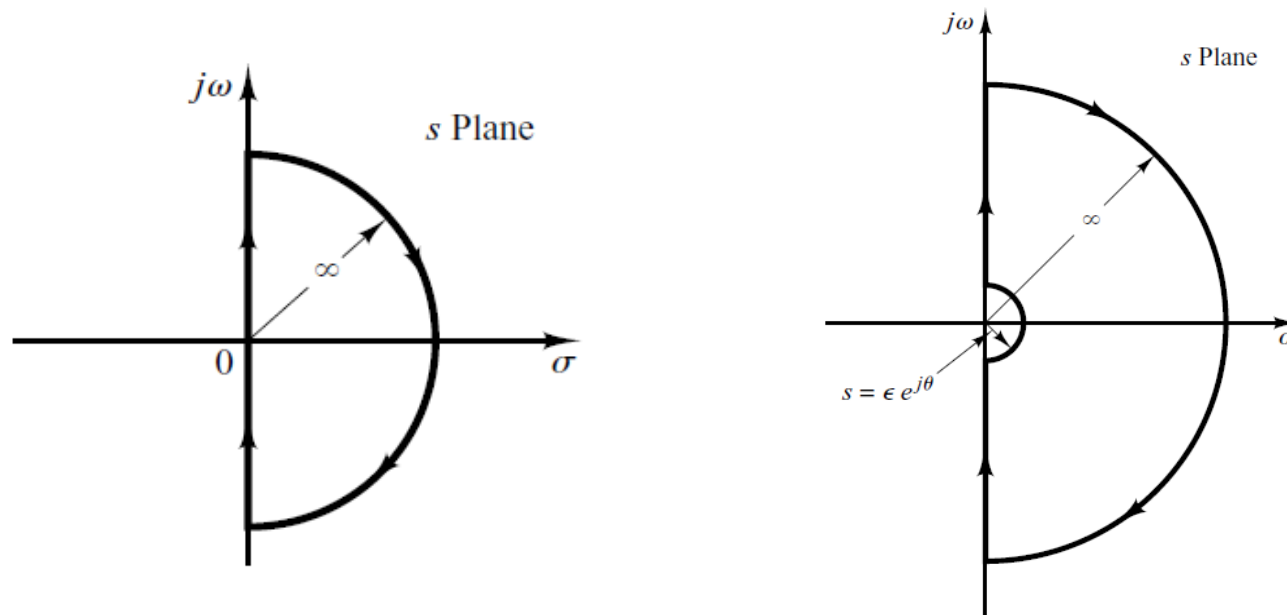
$$\frac{C(s)}{R(s)} = \frac{G(s)}{1 + G(s)H(s)}$$

- For stability, all roots of the characteristic equation, $\Delta(s) = 1 + G(s)H(s) = F(s)$ must lie in the left-half s plane
- The **Nyquist stability criterion** relates the **open-loop frequency response** $G(j\omega)H(j\omega)$ to the number of **zeros and poles** of $\Delta(s)$ of $F(s)$ that lie in the **right-half s plane**
- The absolute stability of the closed-loop system can be determined graphically from open-loop frequency-response curves

Nyquist Stability Criterion

Stability Analysis of Closed-loop Systems

- Let the **closed contour** in the s plane **enclose the entire right-half s plane**
- This contour consists of the entire $j\omega$ axis from $\omega = -\infty$ to $+\infty$ and a semicircular path of infinite radius in the right-half s plane
- The contour encloses all the zeros and poles of $F(s)$ that have positive real parts
- If the function $F(s)$ has poles or zeros at the origin or at some points the $j\omega$ axis, make a **detour** along an infinitesimal semicircle



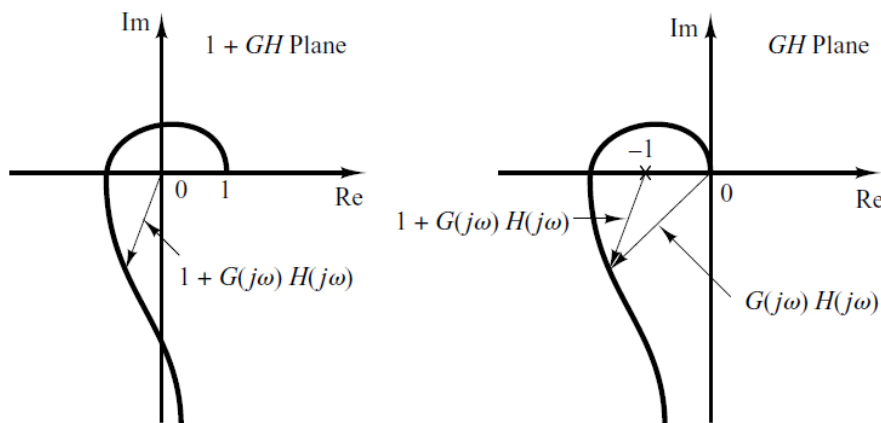
Nyquist Stability Criterion

Stability Analysis of Closed-loop Systems

- If the closed contour in the s plane encloses the entire right-half s plane, then

$$Z = N + P$$

- Z = Number of **right-half s plane zeros** of $F(s)$
 - P = Number of **right-half s plane poles** of $G(s)H(s)$
 - N = Number of **clockwise encirclement of the origin** of the $F(s)$ -plane
- A system is stable, we must have $Z = 0$, or $N = -P$ (having P **counterclockwise** encirclements of the origin)
- The origin of the $F(s)$ -plane is the point $(-1 + j0)$ on the $G(j\omega)H(j\omega)$ plane



Hence, feedback control system is stable if and only if, the number of counterclockwise encirclements of the point $(-1 + j0)$ by the map of the Nyquist contour on the GH -plane = number of poles of the $G(s)H(s)$ within the Nyquist contour on the s plane.

Nyquist Stability Criterion

Practical Approach to Apply the Rule ($Z = N + P$)

- Determine P by inspecting the denominator of the $G(s)H(s)$
- Determine N :
 - Sketch the open-loop locus (**Polar Plot**) from $\omega = -\infty$ to $+\infty$
 - Draw a straight line in any direction from $(-1 + j0)$ point
 - Where this line crosses open-loop locus, mark arrow heads in the direction of increasing frequency
 - $N =$ number of clockwise arrows $-$ number of counterclockwise arrows

Example 6

Consider a closed-loop system whose open-loop transfer function is given by

$$G(s)H(s) = \frac{K}{(T_1s + 1)(T_2s + 1)}$$

with K , T_1 and T_2 are positive values. Examine the stability of the system with the given polar plot.

Answer:

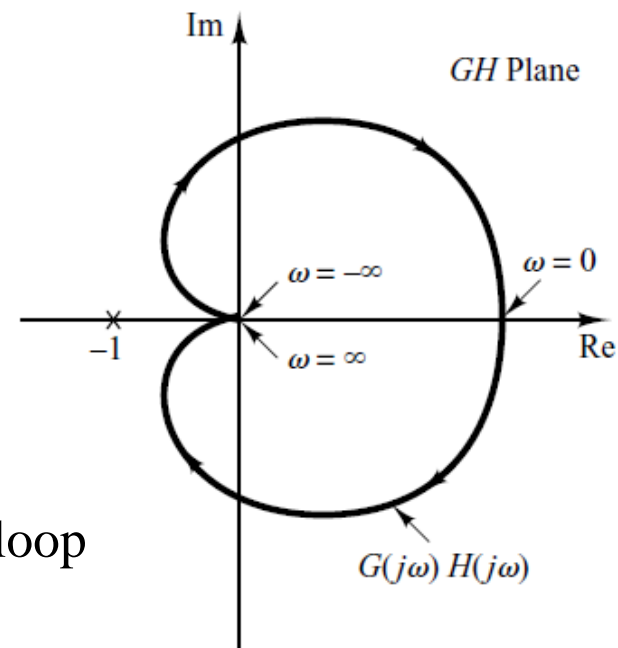
Nyquist Stability Criterion: $Z = N + P$

$$P = 0$$

$$N = 0$$

Hence, $Z = 0$.

The system is **stable** since there is no closed-loop poles in the right-half s plane



Example 7

Consider the system with the following open-loop transfer function,

$$G(s)H(s) = \frac{K}{s(T_1s + 1)(T_2s + 1)}$$

with K , T_1 and T_2 are positive values. Determine the stability of the system for two cases: (1) the gain K is small and (2) K is large.

Answer:

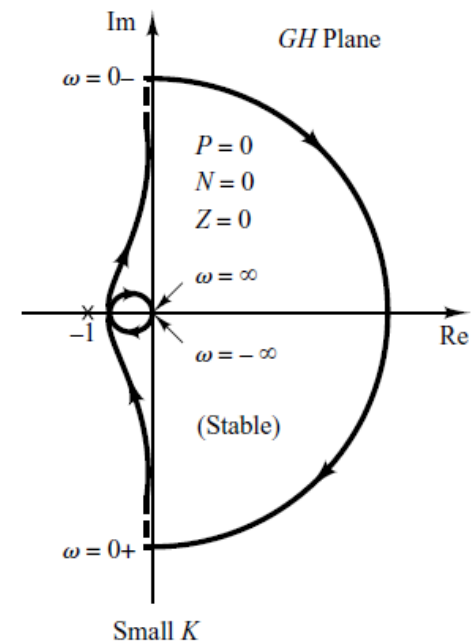
Nyquist Stability Criterion: $Z = N + P$

$P = 0$

$N = 0$

Hence, $Z = 0$.

The system is **stable** since there is no closed-loop poles in the right-half s plane



Example 7

Answer:

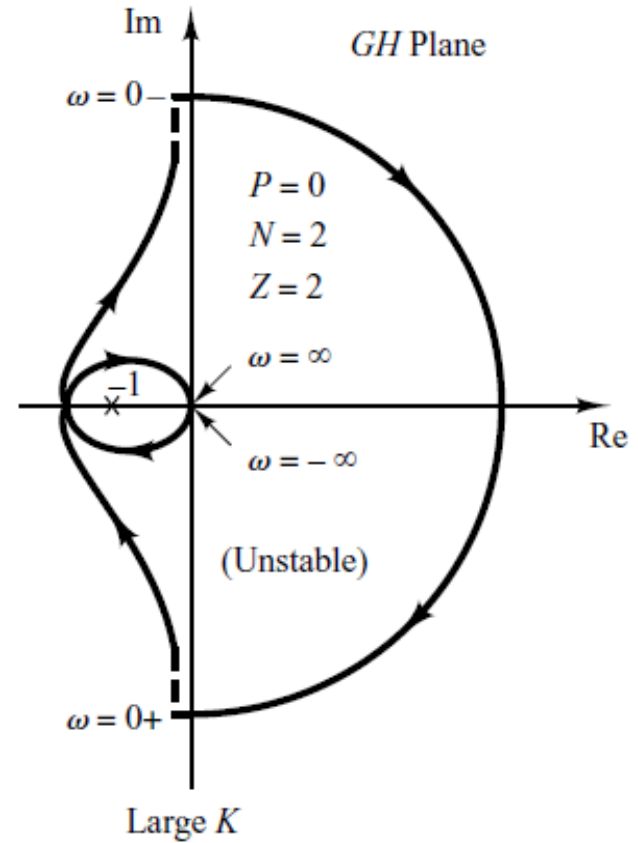
Nyquist Stability Criterion: $Z = N + P$

$P = 0$

$N = 2$ (2 clockwise encirclements of $(-1 + j0)$)

Hence, $Z = 2$.

The system is **unstable** since there is 2 closed-loop poles in the right-half s plane



Relative Stability Analysis

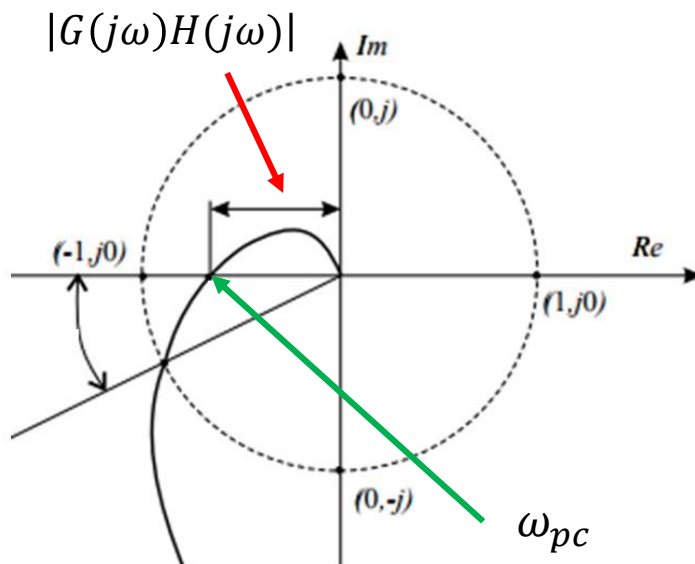
Relative Stability

- The **degree of stability** of a stable system, hence we can think of different design strategies to improve the stability of the control systems
- The **closer** the $G(j\omega)H(j\omega)$ locus comes to encircling the point $(-1 + j0)$, the **more oscillatory** is the system response
- Hence, the **proximity** of the **open-loop frequency response** ($G(j\omega)H(j\omega)$ locus) to the point $(-1 + j0)$ on the GH -plane (or $F(s)$ -plane) is a measure of the **relative stability** of a closed-loop system
- It is a common practice to represent the proximity in terms of **phase margin** and **gain margin**

Relative Stability Analysis

Gain Margin

- It is defined as the **additional gain** required to make the system **just unstable**
- The amount by which the magnitude of $G(j\omega)H(j\omega)$ must be increased in order to be equal to 1 when $\angle G(j\omega)H(j\omega) = -180^\circ$
- **Phase crossover frequency** (ω_{pc}) - the frequency at which $\angle G(j\omega)H(j\omega) = -180^\circ$



$$G.M. = \frac{1}{|G(j\omega)H(j\omega)|}$$

$$G.M. \text{ (dB)} = -20 \log |G(j\omega)H(j\omega)|$$

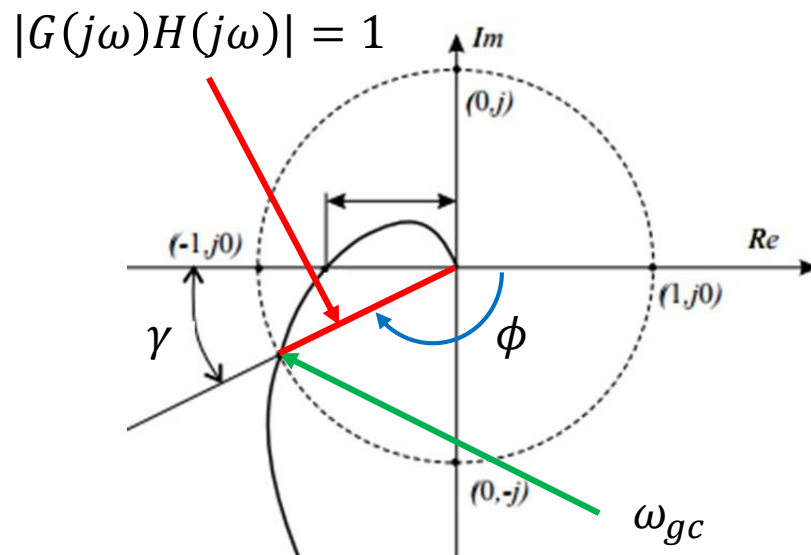
Typical Degree Values

$$G.M. = 1.5 \sim 4.0 \text{ (3.5} \sim 12 \text{ dB)}$$

Relative Stability Analysis

Phase Margin

- It is defined as the **additional phase lag** required to make the system **just unstable**
- The additional phase lag required make $\angle G(j\omega)H(j\omega) = -180^\circ$ at the frequency for which the magnitude of $G(j\omega)H(j\omega)$ is equal to 1
- **Gain crossover frequency** (ω_{gc}) - the frequency at which $|G(j\omega)H(j\omega)| = 1$



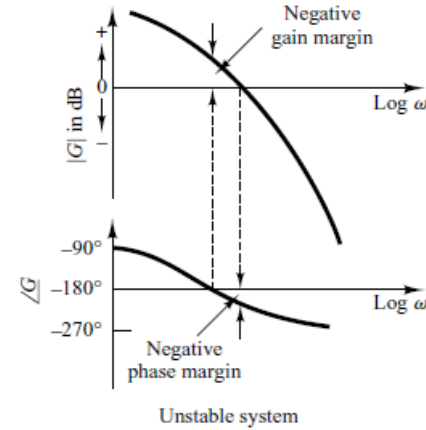
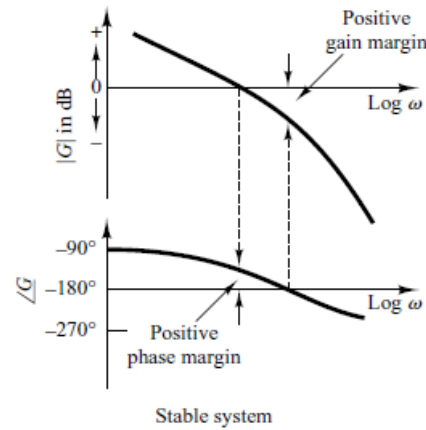
$$P.M. = \gamma = 180^\circ + \angle G(j\omega)H(j\omega)$$

$$\gamma = 180^\circ + \phi$$

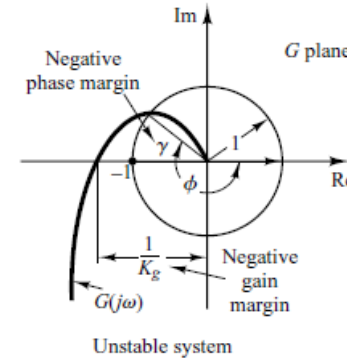
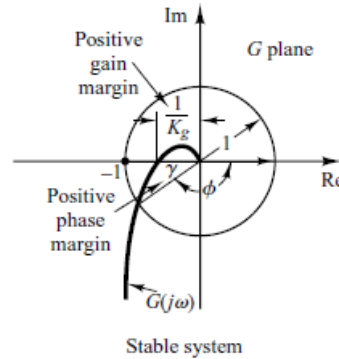
Typical Degree Values

$$P.M. = \gamma = 30^\circ \sim 60^\circ$$

Relative Stability Analysis

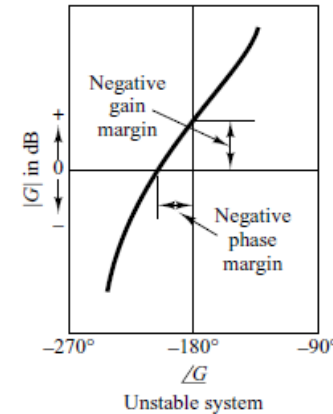
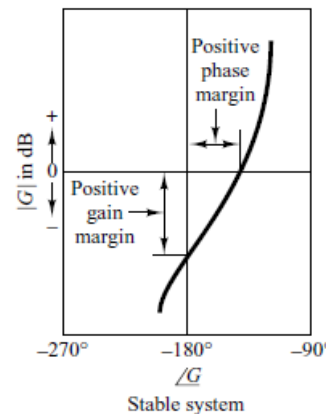


(a)



(b)

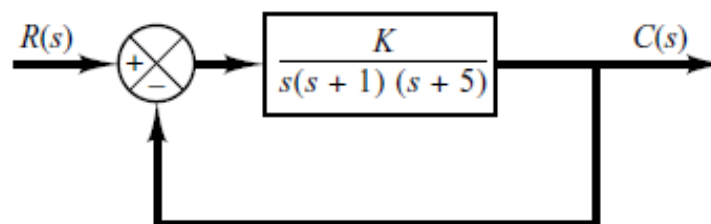
- (a) Bode diagrams
- (b) Polar Plots
- (c) Log-magnitude versus-phase plots



(c)

Example 8

Obtain the phase and gain margins of the system shown below for the two cases where $K = 10$ and $K = 100$.



Answer:

You can either draw the **Bode diagrams, polar plot or Nichols plot** of the **open-loop** frequency response for determining the G.M. and P.M. with the following magnitude and phase equations.

$$G(j\omega) = \frac{K}{j\omega(j\omega + 1)(j\omega + 5)}$$

$$|G(j\omega)|(\text{dB}) = 20 \log K - 20 \log \omega - 20 \log \sqrt{1 + \omega^2} - 20 \log \sqrt{5^2 + \omega^2}$$

$$\angle G(j\omega)(^\circ) = -90^\circ - \tan^{-1} \omega - \tan^{-1} \frac{\omega}{5}$$

Example 8

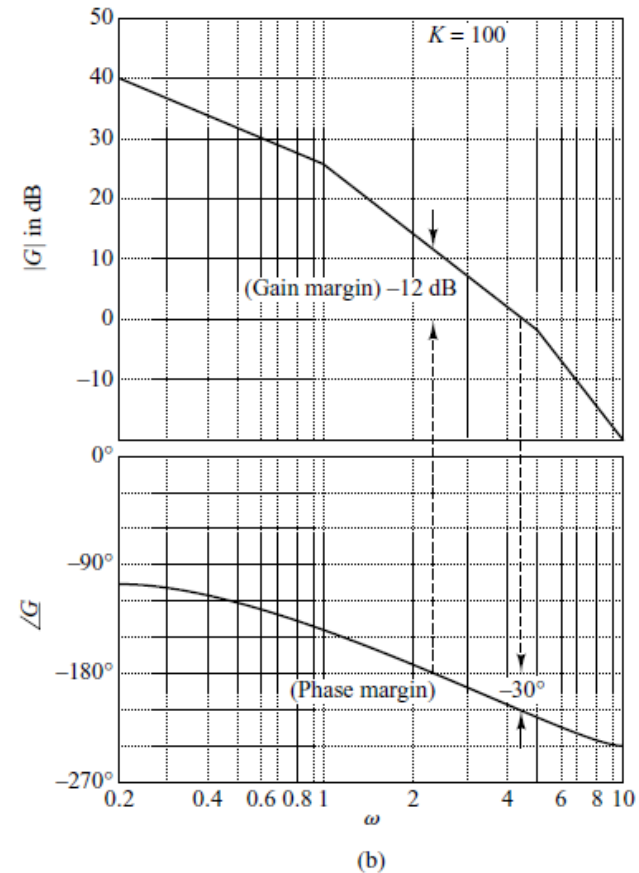
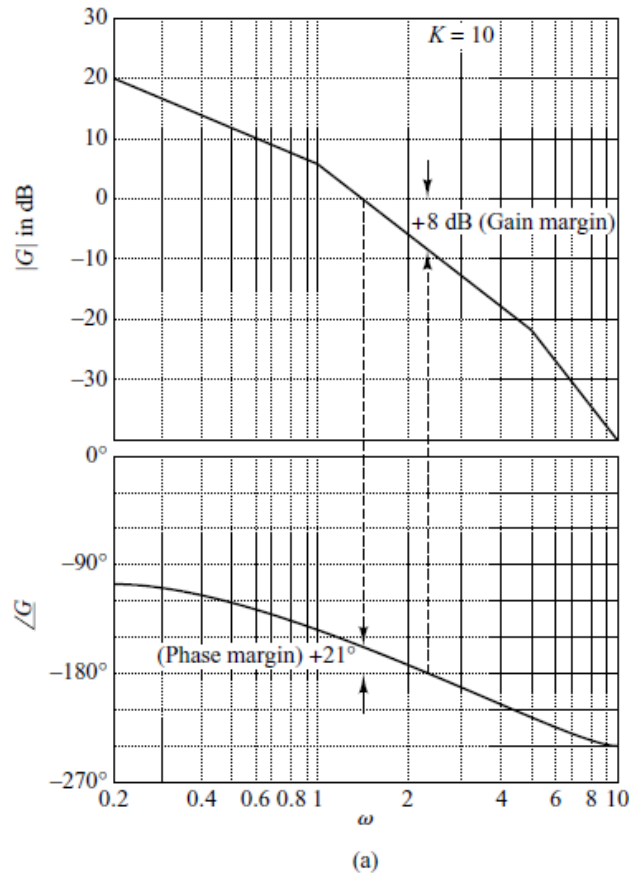
$$|G(j\omega)|(\text{dB}) = 20 \log K - 20 \log \omega - 20 \log \sqrt{1 + \omega^2} - 20 \log \sqrt{5^2 + \omega^2}$$

$$\angle G(j\omega)(^\circ) = -90^\circ - \tan^{-1} \omega - \tan^{-1} \frac{\omega}{5}$$

ω (Rad/s)	$K = 10$		$K = 100$	
	Magnitude (dB)	Phase	Magnitude (dB)	Phase
0.2	19.823	-103.6°	39.823	-103.6°
0.5	11.029	-122.28°	31.029	-122.28°
1	2.84	-146.31°	22.84	-146.31°
2	-7.634	-175.24°	12.37	-175.24°
5	-25.119	-213.7°	-5.119	-213.7°
6	-29.1	-220.73°	-9.1	-220.73°
7	-32.584	-226.33°	-12.584	-226.33°
8	-35.685	-230.87°	-15.685	-230.87°
10	-41.01	-237.72°	-21.01	-237.72°

Example 8

Answer:



The phase and gain margins can easily be obtained from the Bode diagram.

The phase and gain margins for $K = 10$ are P.M. = 21° and G.M. = +8 dB

Therefore, the system gain may be increased by 8 dB before the instability occurs.

The phase and gain margins for $K = 100$ are P.M. = -30° and G.M. = -12 dB

Thus, the system is stable for $K = 10$, but unstable for $K = 100$.

Example 8

Answer:

Beside graphically solved the problem, we can use **analytical method** as below.

$$G(j\omega) = \frac{K}{j\omega(j\omega + 1)(j\omega + 5)}$$

$$\angle G(j\omega)(^\circ) = -90^\circ - \tan^{-1} \omega - \tan^{-1} \frac{\omega}{5}$$

$$|G(j\omega)| = \frac{K}{\omega\sqrt{1 + \omega^2}\sqrt{5^2 + \omega^2}}$$

Gain Margin

When system phase, $\phi = -180^\circ$, and put it into the phase equation, we can find the **phase crossover frequency**, ω_{pc} ,

$$-180^\circ = -90^\circ - \tan^{-1} \omega - \tan^{-1} \frac{\omega}{5}$$

$$90^\circ = \tan^{-1} \omega + \tan^{-1} \frac{\omega}{5}$$

Since $\tan^{-1} X + \tan^{-1} Y = \tan^{-1} \left(\frac{X + Y}{1 - XY} \right)$, hence $\infty = \frac{\omega + \frac{\omega}{5}}{1 - (\omega) \left(\frac{\omega}{5} \right)}$

Example 8

Answer:

Gain Margin

The equation is equal to infinity if and only if the denominator is equal to zero, we have

$$1 - \frac{\omega^2}{5} = 0 \Rightarrow \omega^2 = 5 \Rightarrow \omega = 2.236 \text{ rad/s}$$

The phase crossover frequency, $\omega_{pc} = 2.236 \text{ rad/s}$. Substitute this into the magnitude equation with $K = 10$, we have

$$|G(j\omega)| = \frac{10}{2.236\sqrt{1 + (2.236)^2}\sqrt{5^2 + (2.236)^2}} = 0.3333$$

$$|G(j\omega)| = -20 \log 0.3333 = -9.543 \text{ dB}$$

$$\therefore \text{G.M.} = 0 - (-9.543) = 9.543 \text{ dB}$$

Example 8

Answer:

Phase Margin

When system magnitude, $|G(j\omega)| = 1$ or 0 dB, and put it into the magnitude equation, we can find the **gain crossover frequency**, ω_{gc} , for $K = 10$,

$$1 = \frac{10}{\omega\sqrt{1+\omega^2}\sqrt{5^2+\omega^2}} \Rightarrow \sqrt{\omega^2(1+\omega^2)(25+\omega^2)} = 10$$

So, the equation will be, $\omega^6 + 26\omega^4 + 25\omega^2 - 100 = 0$. Substitute $a = \omega^2$ into the equation, we have

$$a^3 + 26a^2 + 25a - 100 = 0$$

By the solving the equation, we have $a = -2.675$ (rejected), $a = -24.83$ (rejected) and $a = 1.506$. Hence, $\omega^2 = 1.506$, $\omega = \omega_{gc} = 1.227$ rad/s

Put $\omega_{gc} = 1.227$ rad/s into $\angle G(j\omega) = -90^\circ - \tan^{-1} \omega - \tan^{-1} \frac{\omega}{5}$,

$$\angle G(j\omega) = -90^\circ - \tan^{-1} 1.227 - \tan^{-1} \frac{1.227}{5} = -154.61^\circ$$

\therefore P.M. = $180^\circ + (-154.61^\circ) = 25.39^\circ$

Example 8

Answer:

Repeat the same procedures for $K = 100$.

Gain Margin

Since the change of gain K will not affect the phase equation and hence the phase crossover frequency, $\omega_{pc} = 2.236$ rad/s. So, the system gain is,

$$|G(j\omega)| = \frac{100}{2.236\sqrt{1 + (2.236)^2}\sqrt{5^2 + (2.236)^2}} = 3.3335$$

$$|G(j\omega)| = 20 \log 3.3335 = 10.46 \text{ dB}$$

$$\therefore \text{G.M.} = 0 - 10.46 = -10.46 \text{ dB}$$

Phase Margin

We need to recalculate the gain crossover frequency, ω_{gc} , for the new gain K .

$$1 = \frac{100}{\omega\sqrt{1 + \omega^2}\sqrt{5^2 + \omega^2}}$$

Hence, we have $\omega_{gc} = 3.907$ rad/s. Put $\omega_{gc} = 3.907$ rad/s into $\angle G(j\omega)$, we have

$$\angle G(j\omega) = -90^\circ - \tan^{-1} 3.907 - \tan^{-1} \frac{3.907}{5} = -203.65^\circ$$

$$\therefore \text{P.M.} = 180^\circ + (-203.65^\circ) = -23.65^\circ$$